

3A, 36V, Synchronous Step-Down Converter

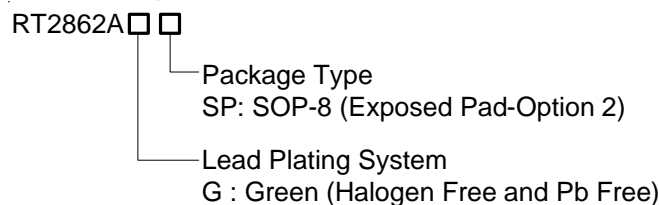
General Description

The RT2862A is a high efficiency, current-mode synchronous step-down DC-DC converter that can deliver up to 3A output current over a wide input voltage range from 4.5V to 36V. The device integrates 105mΩ high-side and 80mΩ low-side MOSFETs to achieve high conversion efficiency. The current-mode control architecture supports fast transient response and simple external compensation.

A cycle-by-cycle current limit function provides protection against shorted output and an internal soft-start eliminates input current surge during start-up. The RT2862A provides complete protection functions such as input under-voltage lockout, output under-voltage protection, over-current protection and thermal shutdown.

The RT2862A is available in the thermal enhanced SOP-8 (Exposed Pad) package.

Ordering Information



Note :

Richtek products are :

- ▶ RoHS compliant and compatible with the current requirements of IPC/JEDEC J-STD-020.
- ▶ Suitable for use in SnPb or Pb-free soldering processes.

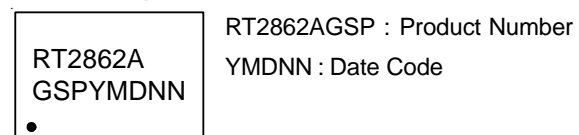
Features

- 4.5V to 36V Input Voltage Range
- 3A Output Current
- Internal N-MOSFETs
- Current Mode Control
- Frequency Operation : 300kHz to 1MHz
- Adjustable Output Voltage from 0.8V to 30V
- High Efficiency Up to 95%
- Stable with Low ESR Ceramic Output Capacitors
- Cycle-by-Cycle Current Limit
- Input Under-Voltage Lockout
- Output Under-Voltage Protection
- Thermal Shutdown
- Power Saving at Light Load

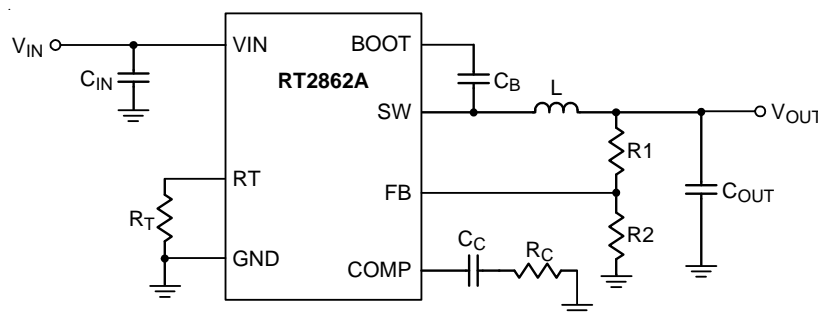
Applications

- Point of Load Regulator in Distributed Power Systems
- Digital Set Top Boxes
- Broadband Communications
- Vehicle Electronics
- Automotive Audio, Navigation, and Information Systems
- Enterprise Datacom Platforms Point of Load (POL)
- Industrial Grade General Purpose Point of Load

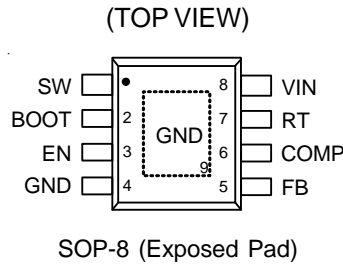
Marking Information



Simplified Application Circuit



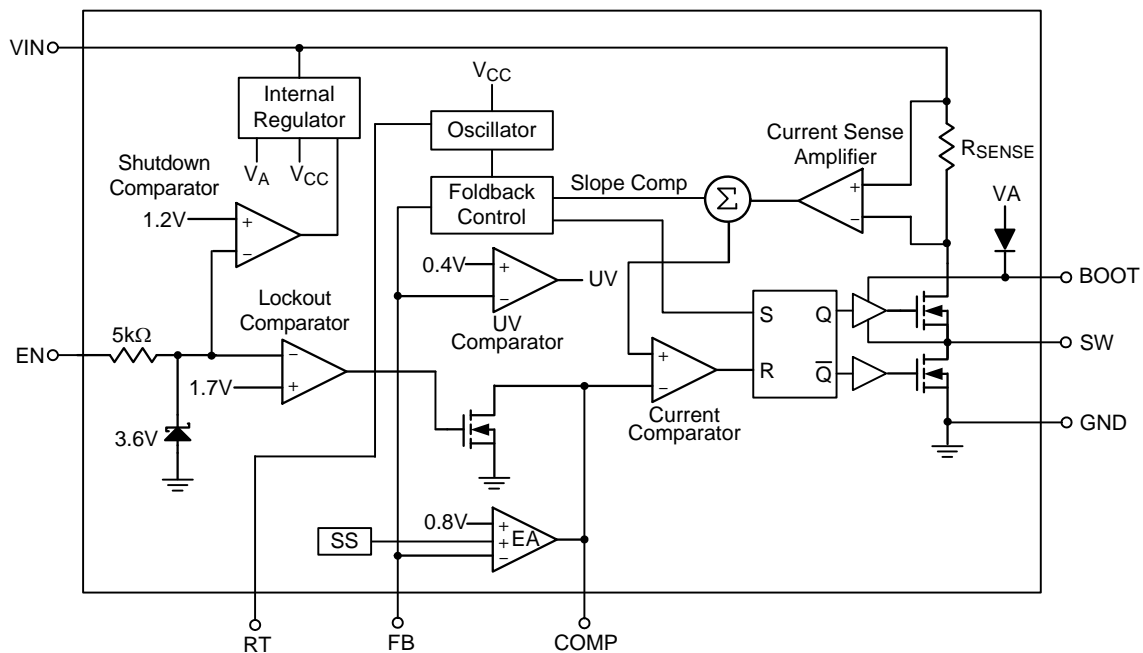
Pin Configuration



Functional Pin Description

Pin No.	Pin Name	Pin Function
1	SW	Switch Node. Connect to external L-C filter.
2	BOOT	Bootstrap Supply for the High-Side MOSFET. Connect a 100nF or greater capacitor between the BOOT and SW pins.
3	EN	Enable Control Input. A logic-high enables the converter; a logic-low forces the device into shutdown mode.
4, 9 (Exposed Pad)	GND	Ground. The exposed pad must be soldered to a large PCB and connected to GND for maximum thermal dissipation.
5	FB	Feedback Voltage Input. This pin is used to set the output voltage of the converter to regulate to the desired value via an resistive divider.
6	COMP	Compensation Node. COMP is used to compensate the regulation control loop. Connect a R-C network from the COMP to GND. In some cases, an additional capacitor from COMP to GND is required.
7	RT	Switching Frequency Setting. Connect an external resistor to set the switching frequency from 300kHz to 1MHz.
8	VIN	Power Input. The input voltage range is from 4.5V to 36V. Must bypass with a suitable large ceramic capacitor at this pin.

Functional Block Diagram



Operation

The RT2862A is a current-mode synchronous step-down converter. In normal operation, the high-side N-MOSFET is turned on when the S-R latch is set by the oscillator and is turned off when the current comparator resets the S-R latch. While the high-side N-MOSFET is turned off, the low-side N-MOSFET is turned on to conduct the inductor current until next cycle begins.

Error Amplifier

The error amplifier adjusts its output voltage by comparing the feedback signal (V_{FB}) with the internal 0.8V reference. When the load current increases, it causes a drop in the feedback voltage relative to the reference, and then the error amplifier's output voltage rises to allow higher inductor current to match the load current.

Oscillator

The oscillator frequency can be set by using an external resistor R_T . Oscillator frequency range is from 300kHz to 1MHz.

Internal Regulator

The regulator provides low voltage power to supply the internal control circuits and the bootstrap power for high-side gate driver.

Enable

The converter is turned on when the EN pin is higher than 2V. When the EN pin is lower than 0.4V, the converter will enter shutdown mode and reduce the supply current to 0.5 μ A.

Soft-Start (SS)

An internal current source charges an internal capacitor to build a soft-start ramp voltage. The FB voltage will track the internal ramp voltage during soft-start interval. The typical soft-start time is 2ms.

UV Comparator

If the feedback voltage is lower than 0.4V, the UV Comparator will go high to turn off the high-side MOSFET. The output under voltage protection is designed to operate in hiccup mode. When the UV condition is removed, the converter will resume switching.

Thermal Shutdown

The over-temperature protection function will shut down the switching operation when the junction temperature exceeds 150°C. Once the junction temperature cools down by approximately 20°C, the converter will automatically resume switching.

Absolute Maximum Ratings (Note 1)

- Supply Voltage, V_{IN} ----- -0.3V to 40V
- Switch Voltage, SW ----- -0.3V to ($V_{IN} + 0.3V$)
- BOOT Pin ----- -0.3V to 46.3V
- EN Pin (with REN (150k Ω to 600k Ω) to V_{IN}) ----- -0.3V to 40V
- SW Voltage ($t < 10ns$) ----- -5V to 46.3V
- EN Pin ----- -0.3V to 3.6V
- Other Pins ----- -0.3V to 40V
- Power Dissipation, P_D @ $T_A = 25^\circ C$
 - SOP-8 (Exposed Pad) ----- 2.041W
- Package Thermal Resistance (Note 2)
 - SOP-8 (Exposed Pad), θ_{JA} ----- 49 $^\circ C/W$
 - SOP-8 (Exposed Pad), θ_{JC} ----- 8 $^\circ C/W$
- Lead Temperature (Soldering, 10 sec.) ----- 260 $^\circ C$
- Junction Temperature ----- 150 $^\circ C$
- Storage Temperature Range ----- -65 $^\circ C$ to 150 $^\circ C$
- ESD Susceptibility (Note 3)
 - HBM (Human Body Model) ----- 2kV

Recommended Operating Conditions (Note 4)

- Supply Input Voltage, V_{IN} ----- 4.5V to 36V
- Junction Temperature Range ----- -40 $^\circ C$ to 125 $^\circ C$
- Ambient Temperature Range ----- -40 $^\circ C$ to 85 $^\circ C$

Electrical Characteristics

($V_{IN} = 12V$, $C_{IN} = 20\mu F$, $T_A = -40^\circ C$ to 85 $^\circ C$, unless otherwise specified)

Parameter	Symbol	Test Conditions	Min	Typ	Max	Unit
Shutdown Supply Current		$V_{EN} = 0V$	--	--	10	μA
Quiescent Current	I_Q	$V_{EN} = 3V$, $V_{FB} = 0.9V$	--	1	1.3	mA
Feedback Reference Voltage	V_{REF}	$4.5V \leq V_{IN} \leq 36V$	0.784	0.8	0.816	V
Switch On-Resistance	High-Side	$R_{DS(ON)1}$	--	105	190	m Ω
	Low-Side	$R_{DS(ON)2}$	--	80	145	
High-Side Switch Current Limit Range	U_{OC}		4.25	5	5.75	A
Low-Side Switch Current Limit		From Drain to Source	--	1.7	--	A
Oscillation Frequency	f_{OSC1}	$R_T = 191k\Omega$	282	320	358	kHz
		$R_T = 113k\Omega$	467	530	593	
		$R_T = 51k\Omega$	924	1050	1176	
Short-Circuit Oscillation Frequency	f_{OSC2}	$V_{FB} = 0V$, $R_T = 113k\Omega$	--	50	--	kHz
Maximum Duty Cycle	D_{MAX}	$V_{FB} = 0.7V$	--	95	--	%
Minimum On-Time	t_{ON}		--	100	120	ns

Parameter		Symbol	Test Conditions	Min	Typ	Max	Unit
EN Input Voltage	Logic-High	V_{IH}		2	--	3.3	V
	Logic-Low	V_{IL}		--	--	0.4	
Input Under-Voltage Lockout Threshold		V_{UVLO}	V_{IN} Rising	3.7	4.2	4.5	V
Input Under-Voltage Lockout Hysteresis		ΔV_{UVLO}		--	250	--	mV
Thermal Shutdown Threshold		T_{SD}		--	150	--	°C
Thermal Shutdown Hysteresis		ΔT_{SD}		--	25	--	°C
COMP to Current Sense Trans-conductance		G_{CS}	$\Delta I_{COMP} = \pm 10\mu A$	--	4.1	--	A/V
Error Amplifier Trans-conductance		G_{EA}		--	950	--	$\mu A/V$

- Note 1.** Stresses beyond those listed “Absolute Maximum Ratings” may cause permanent damage to the device. These are stress ratings only, and functional operation of the device at these or any other conditions beyond those indicated in the operational sections of the specifications is not implied. Exposure to absolute maximum rating conditions may affect device reliability.
- Note 2.** θ_{JA} is measured at $T_A = 25\text{ °C}$ on a high effective thermal conductivity four-layer test board per JEDEC 51-7. θ_{JC} is measured at the exposed pad of the package. The PCB copper area with exposed pad is 70mm^2 .
- Note 3.** Devices are ESD sensitive. Handling precaution is recommended.
- Note 4.** The device is not guaranteed to function outside its operating conditions.

Typical Application Circuit

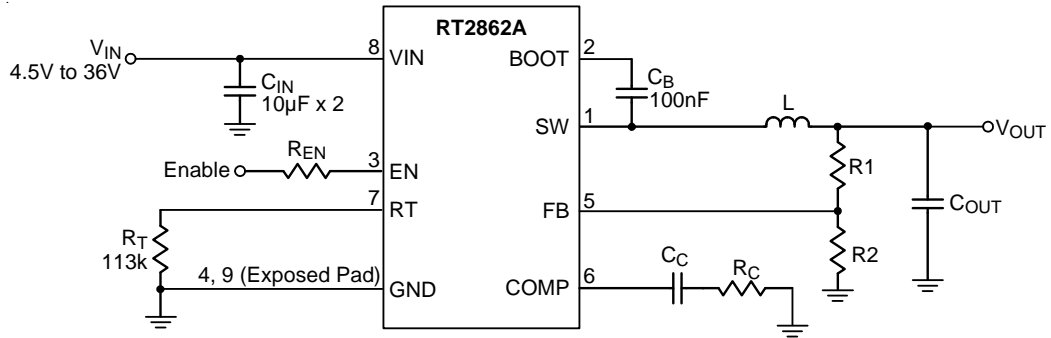
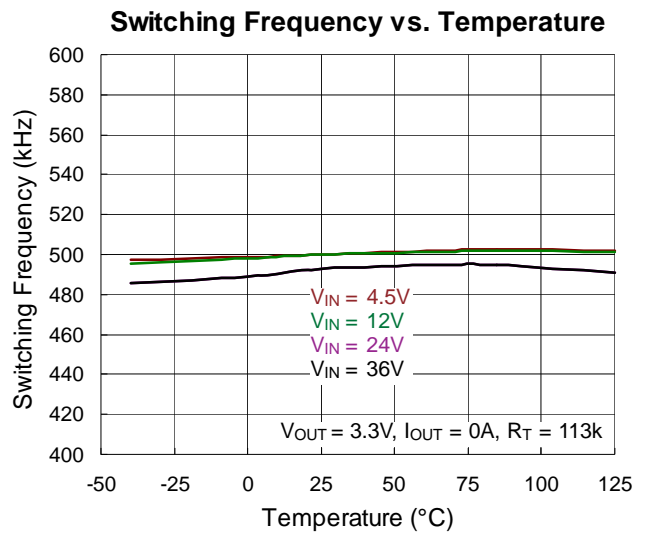
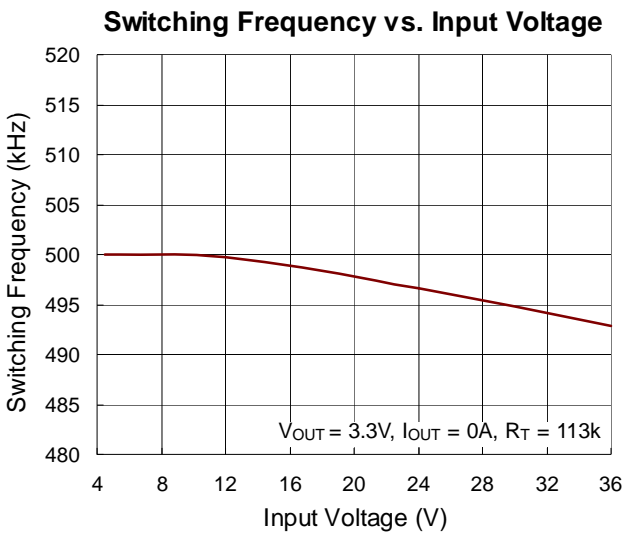
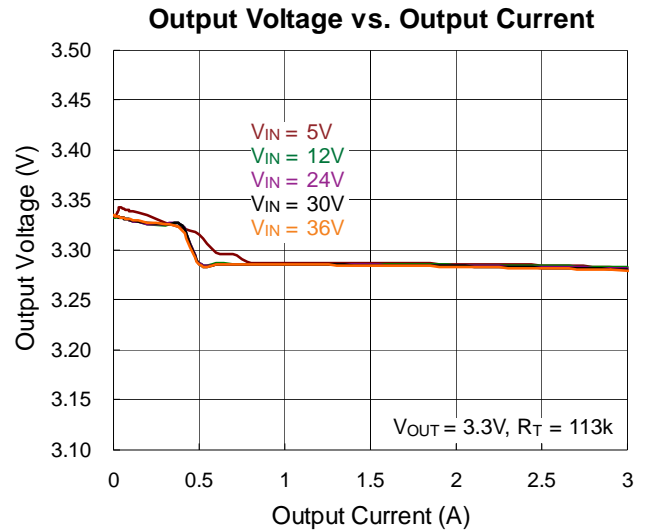
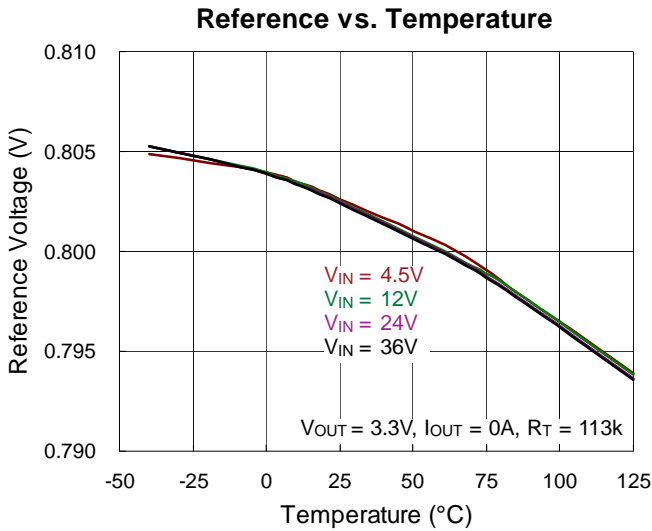
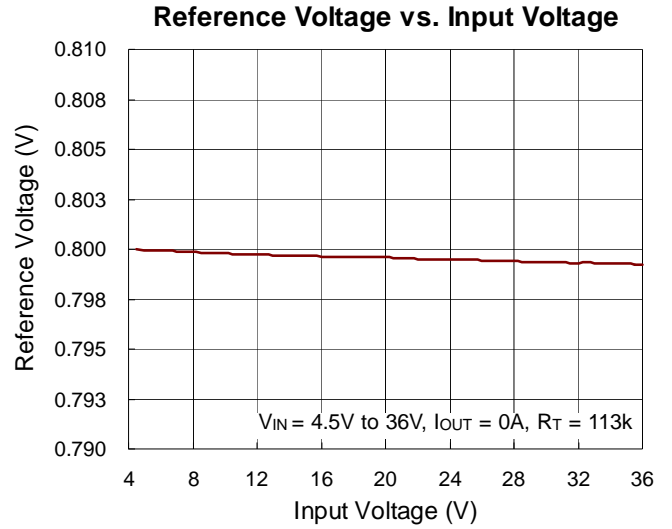
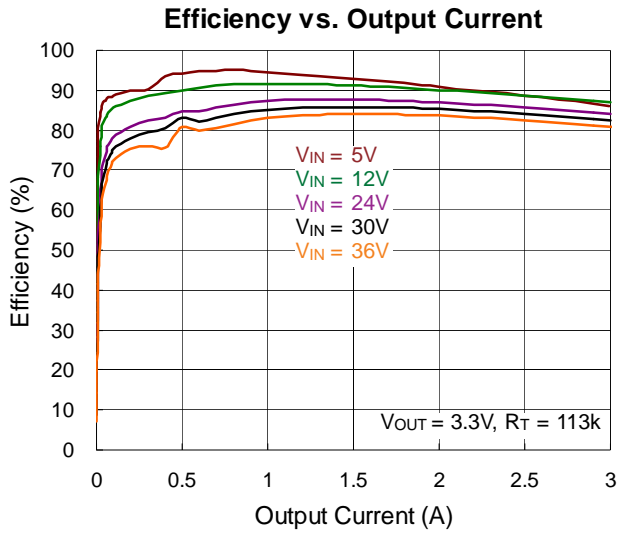


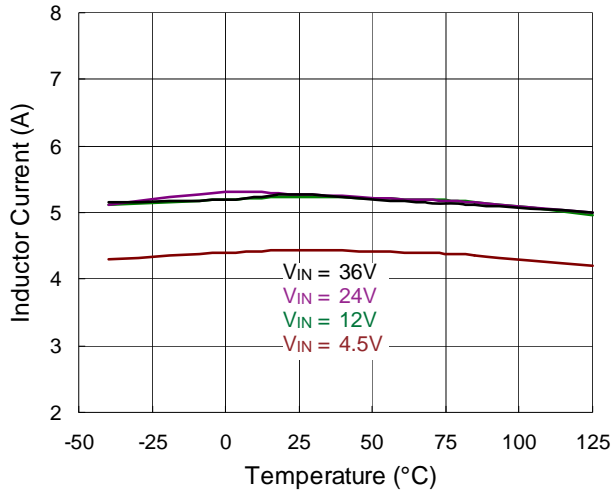
Table 1. Suggested Component Values

V _{OUT} (V)	R ₁ (kΩ)	R ₂ (kΩ)	R _C (kΩ)	L (µH)	C _C (nF)	C _{OUT} (µF)
12	47	3.35	47	10	2.7	22 x 2
8	27	3	36	8.2	2.7	22 x 2
5	62	11.8	24	6.8	2.7	22 x 2
3.3	75	24	16	4.7	2.7	22 x 2
2.5	25.5	12	12	3.6	2.7	22 x 2
1.2	30	60	6.8	2.2	2.7	22 x 2

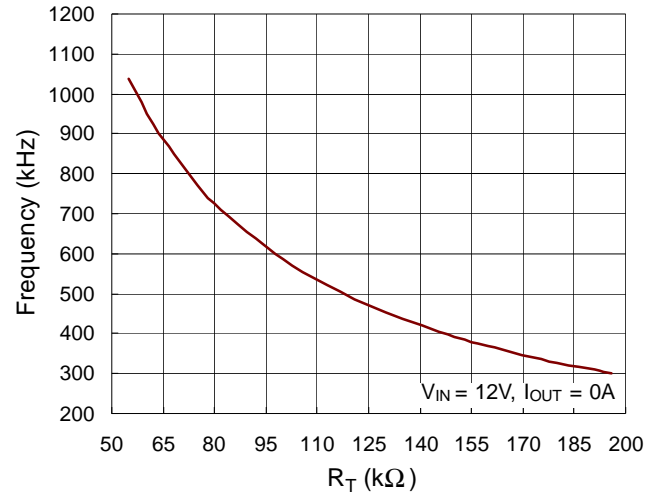
Typical Operating Characteristics



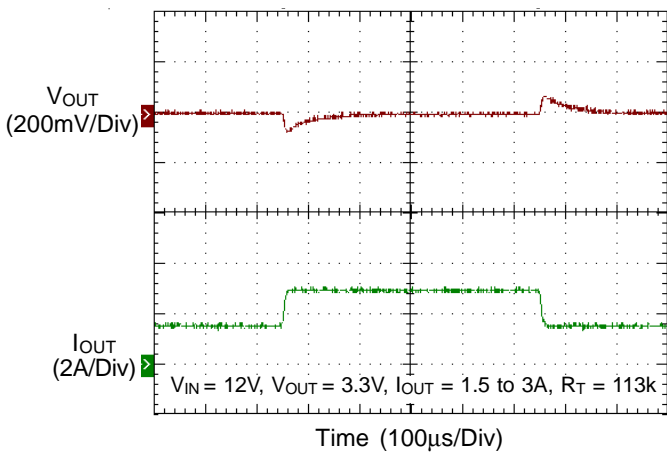
Current Limit vs. Temperature



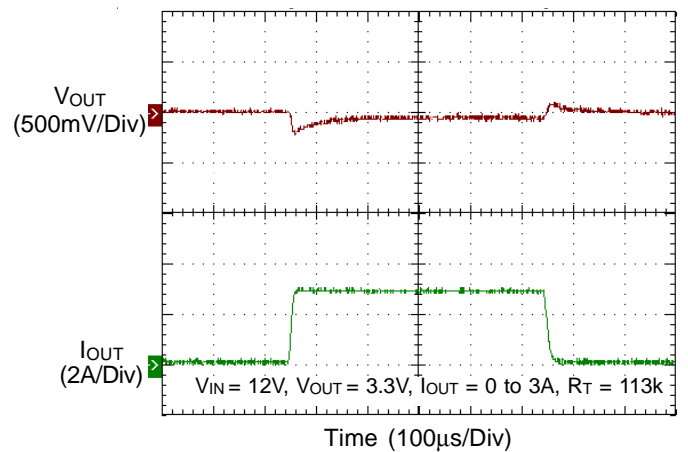
Frequency vs. R_T



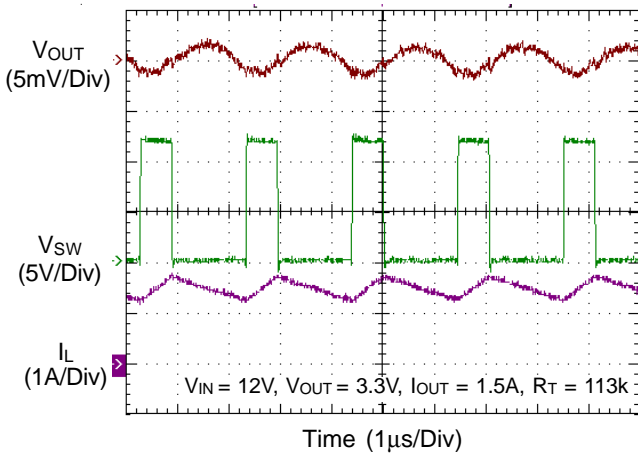
Load Transient Response



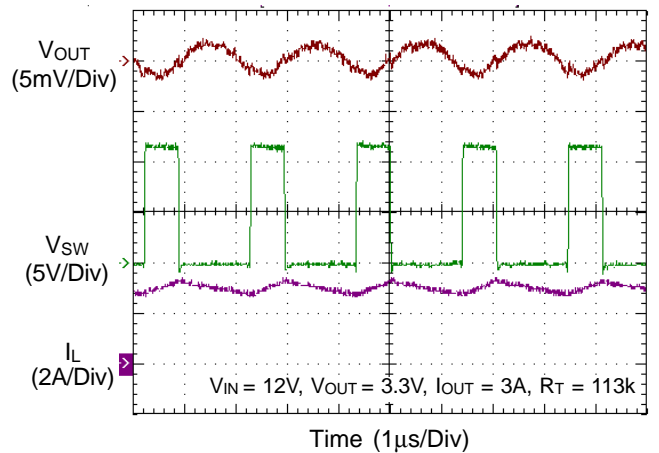
Load Transient Response



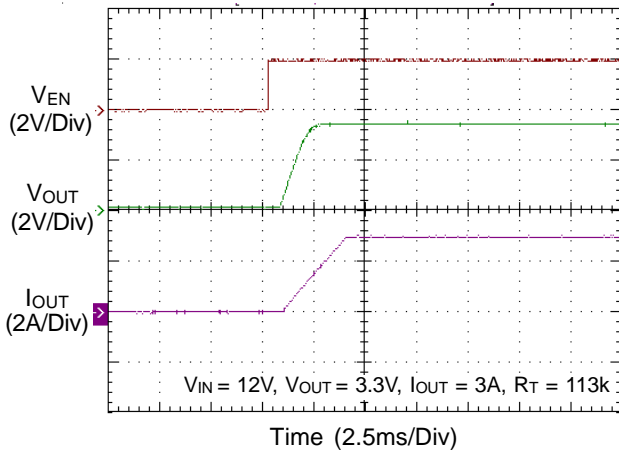
Switching



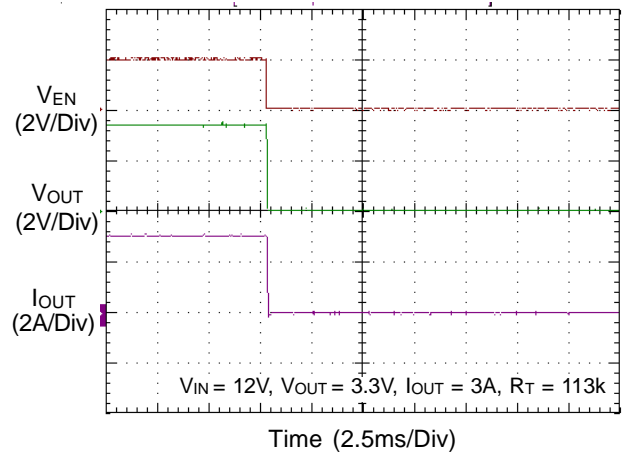
Switching



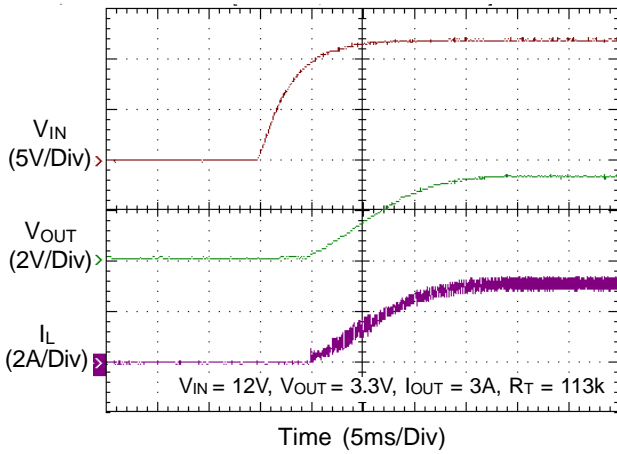
Power On from EN



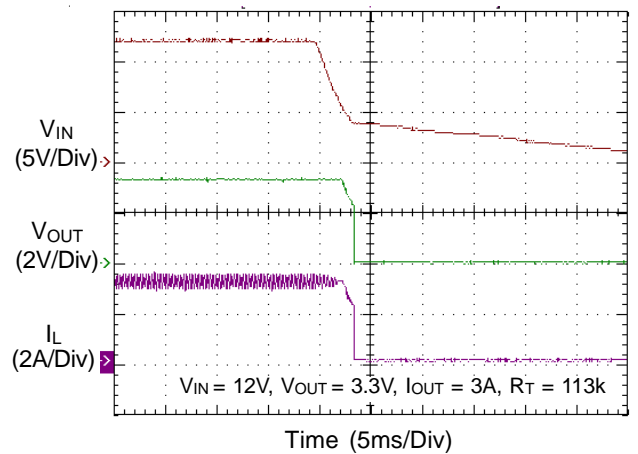
Power Off from EN



Power On from VIN



Power Off from VIN



Application Information

Output Voltage Setting

The resistive divider allows the FB pin to sense the output voltage as shown in Figure 1.

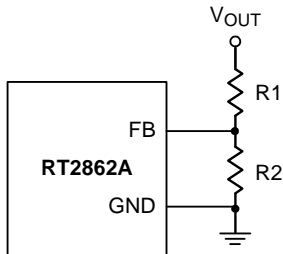


Figure 1. Output Voltage Setting

The output voltage is set by an external resistive voltage divider according to the following equation :

$$V_{OUT} = V_{REF} \left(1 + \frac{R1}{R2} \right)$$

where V_{REF} is the reference voltage (0.8V typ.).

External Bootstrap Diode

Connect a 0.1μF low ESR ceramic capacitor between the BOOT and SW pins. This capacitor provides the gate driver voltage for the high-side MOSFET.

It is recommended to add an external bootstrap diode between an external 5V and BOOT pin for efficiency improvement when input voltage is lower than 5.5V or duty ratio is higher than 65% .The bootstrap diode can be a low cost one such as IN4148 or BAT54. The external 5V can be a 5V fixed input from system or a 5V output of the RT2862A. Note that the external boot voltage must be lower than 5.5V

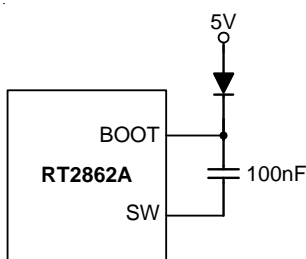


Figure 2. External Bootstrap Diode

Chip Enable Operation

The EN pin is the chip enable input. Pulling the EN pin low (<0.4V) will shutdown the device. During shutdown mode, the RT2862A quiescent current drops to lower than 3μA. Driving the EN pin high (>2.5V, <3.3V) will turn on the device again. For external timing control, the EN pin can also be externally pulled high by adding a R_{EN} resistor and C_{EN} capacitor from the V_{IN} pin (see Figure 3).

R_{EN} must be chose between 150kΩ to 600kΩ, which is to avoid huge leak current into chip.

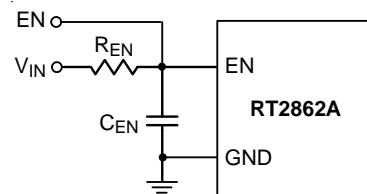


Figure 3. Enable Timing Control

An external MOSFET can be added to implement digital control on the EN pin when no system voltage above 2.5V is available, as shown in Figure 4. In this case, a 300kΩ pull-up resistor, R_{EN} , is connected between V_{IN} and the EN pin. MOSFET Q1 will be under logic control to pull down the EN pin.

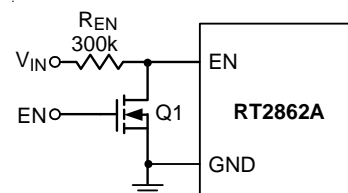


Figure 4. Digital Enable Control Circuit

Under-Voltage Protection

Hiccup Mode

The RT2862A provides Hiccup Mode Under-Voltage Protection (UVP). When the V_{FB} voltage drops below 0.4V, the UVP function will be triggered to shut down switching operation. If the UVP condition remains for a period, the RT2862A will retry automatically. When the UVP condition is removed, the converter will resume operation. The UVP is disabled during soft-start period.

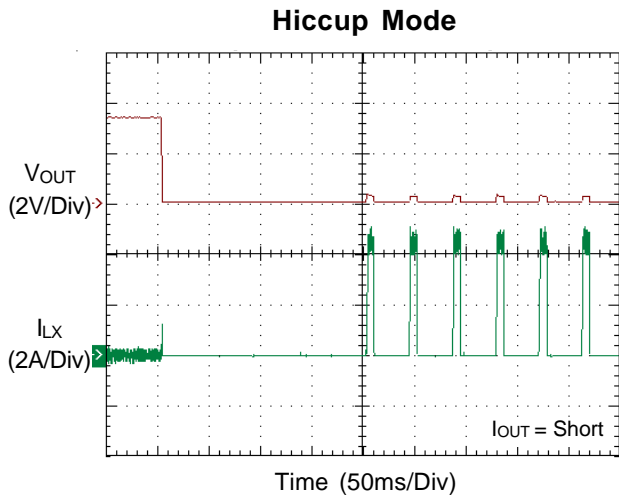


Figure 5. Hiccup Mode Under-Voltage Protection

Over-Temperature Protection

The RT2862A features an Over-Temperature Protection (OTP) circuitry to prevent overheat due to excessive power dissipation. The OTP will shut down switching operation when junction temperature exceeds 150°C. Once the junction temperature cools down by approximately 20°C, the converter will resume operation. To maintain continuous operation, the maximum junction temperature should be lower than 125°C.

Inductor Selection

The inductor value and operating frequency determine the ripple current according to a specific input and output voltage. The ripple current ΔI_L increases with higher V_{IN} and decreases with higher inductance.

$$\Delta I_L = \left[\frac{V_{OUT}}{f \times L} \right] \times \left[1 - \frac{V_{OUT}}{V_{IN}} \right]$$

Having a lower ripple current reduces not only the ESR losses in the output capacitors but also the output voltage ripple. High frequency with small ripple current can achieve the highest efficiency operation. However, it requires a large inductor to achieve this goal.

For the ripple current selection, the value of $\Delta I_L = 0.24(I_{MAX})$ will be a reasonable starting point. The largest ripple current occurs at the highest V_{IN} . To guarantee that the ripple current stays below the specified maximum, the inductor value should be chosen according to the following equation :

$$L = \left[\frac{V_{OUT}}{f \times \Delta I_L(MAX)} \right] \times \left[1 - \frac{V_{OUT}}{V_{IN(MAX)}} \right]$$

The inductor's current rating (caused a 40°C temperature rising from 25°C ambient) should be greater than the maximum load current and its saturation current should be greater than the short circuit peak current limit. Please see Table 2 for the inductor selection reference.

Table 2. Suggested Inductors for Typical Application Circuit

Component Supplier	Series	Dimensions (mm)
TDK	VLF10045	10 x 9.7 x 4.5
TDK	SLF12565	12.5 x 12.5 x 6.5
TAIYO YUDEN	NR8040	8 x 8 x 4

C_{IN} and C_{OUT} Selection

The input capacitance, C_{IN} , is needed to filter the trapezoidal current at the Source of the high-side MOSFET. To prevent large ripple current, a low ESR input capacitor sized for the maximum RMS current should be used. The approximate RMS current equation is given :

$$I_{RMS} = I_{OUT(MAX)} \frac{V_{OUT}}{V_{IN}} \sqrt{\frac{V_{IN}}{V_{OUT}} - 1}$$

This formula has a maximum at $V_{IN} = 2V_{OUT}$, where $I_{RMS} = I_{OUT} / 2$. This simple worst case condition is commonly used for design because even significant deviations do not offer much relief.

Choose a capacitor rated at a higher temperature than required. Several capacitors may also be paralleled to meet size or height requirements in the design.

For the input capacitor, two 10μF low ESR ceramic capacitors are suggested. For the suggested capacitor, please refer to Table 3 for more details.

The selection of C_{OUT} is determined by the required ESR to minimize voltage ripple.

Moreover, the amount of bulk capacitance is also a key for C_{OUT} selection to ensure that the control loop is stable. Loop stability can be checked by viewing the load transient response as described in a later section.

The output ripple, ΔV_{OUT} , is determined by :

$$\Delta V_{OUT} \leq \Delta I_L \left[ESR + \frac{1}{8fC_{OUT}} \right]$$

The output ripple will be the highest at the maximum input voltage since ΔI_L increases with input voltage. Multiple capacitors placed in parallel may be needed to meet the ESR and RMS current handling requirement. Higher values, lower cost ceramic capacitors are now becoming available in smaller case sizes. Their high ripple current, high voltage rating and low ESR make them ideal for switching regulator applications. However, care must be taken when these capacitors are used at input and output. When a ceramic capacitor is used at the input and the power is supplied by a wall adapter through long wires, a load step at the output can induce ringing at the input, V_{IN} . At best, this ringing can couple to the output and be mistaken as loop instability. At worst, a sudden inrush of current through the long wires can potentially cause a voltage spike at V_{IN} large enough to damage the part.

Thermal Considerations

For continuous operation, do not exceed the maximum operation junction temperature 125°C . The maximum power dissipation depends on the thermal resistance of IC package, PCB layout, the rate of surroundings airflow and temperature difference between junction to ambient. The maximum power dissipation can be calculated by following formula :

$$P_{D(MAX)} = (T_{J(MAX)} - T_A) / \theta_{JA}$$

Where $T_{J(MAX)}$ is the maximum operation junction temperature , T_A is the ambient temperature and the θ_{JA} is the junction to ambient thermal resistance.

For recommended operating conditions specification of RT2862A, the maximum junction temperature is 125°C . The junction to ambient thermal resistance θ_{JA} is layout dependent. For SOP-8 (Exposed Pad) package, the thermal resistance θ_{JA} is 75°C/W on the standard JEDEC 51-7 four-layers thermal test board. The maximum power dissipation at $T_A = 25^{\circ}\text{C}$ can be calculated by following formula :

$$P_{D(MAX)} = (125^{\circ}\text{C} - 25^{\circ}\text{C}) / (75^{\circ}\text{C/W}) = 1.333\text{W}$$

(min.copper area PCB layout)

$$P_{D(MAX)} = (125^{\circ}\text{C} - 25^{\circ}\text{C}) / (49^{\circ}\text{C/W}) = 2.04\text{W}$$

(70mm^2 copper area PCB layout)

The thermal resistance θ_{JA} of SOP-8 (Exposed Pad) is determined by the package architecture design and the PCB layout design. However, the package architecture design had been designed. If possible, it's useful to increase thermal performance by the PCB layout copper design. The thermal resistance θ_{JA} can be decreased by adding copper area under the exposed pad of SOP-8 (Exposed Pad) package.

As shown in Figure 6, the amount of copper area to which the SOP-8 (Exposed Pad) is mounted affects thermal performance. When mounted to the standard SOP-8 (Exposed Pad) pad (Figure 6.a), θ_{JA} is 75°C/W . Adding copper area of pad under the SOP-8 (Exposed Pad) (Figure 6.b) reduces the θ_{JA} to 64°C/W . Even further, increasing the copper area of pad to 70mm^2 (Figure 6.e) reduces the θ_{JA} to 49°C/W .

The maximum power dissipation depends on operating ambient temperature for fixed $T_{J(MAX)}$ and thermal resistance θ_{JA} . The Figure 7 of derating curves allows the designer to see the effect of rising ambient temperature on the maximum power dissipation allowed.

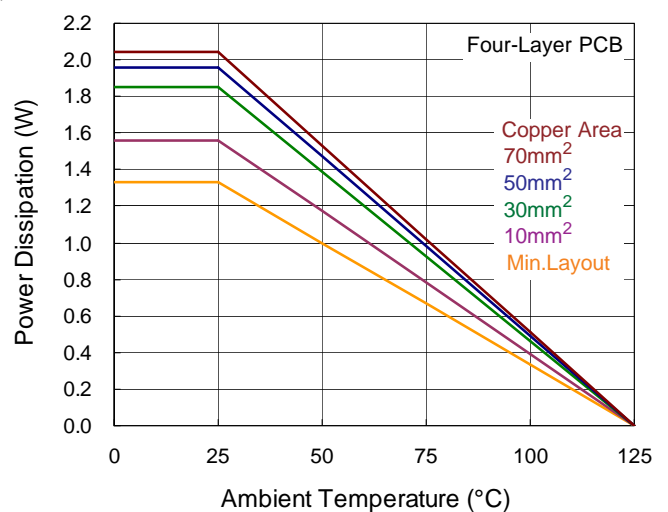
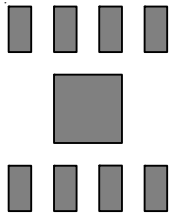
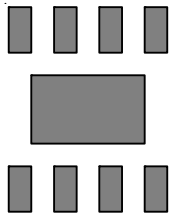


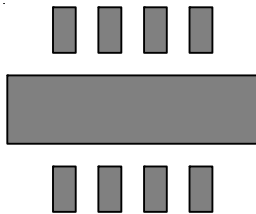
Figure 7. Derating Curve of Maximum Power Dissipation



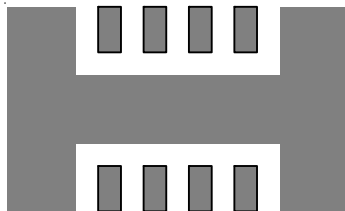
(a) Copper Area = $(2.3 \times 2.3) \text{ mm}^2$, $\theta_{JA} = 75^\circ\text{C/W}$



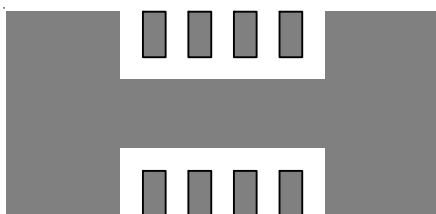
(b) Copper Area = 10mm^2 , $\theta_{JA} = 64^\circ\text{C/W}$



(c) Copper Area = 30mm^2 , $\theta_{JA} = 54^\circ\text{C/W}$



(d) Copper Area = 50mm^2 , $\theta_{JA} = 51^\circ\text{C/W}$



(e) Copper Area = 70mm^2 , $\theta_{JA} = 49^\circ\text{C/W}$

Figure 6. Thermal Resistance vs. Copper Area Layout Design

Layout Considerations

For best performance of the RT2862A, the following layout guidelines must be strictly followed.

- ▶ Input capacitor must be placed as close to the IC as possible.
- ▶ SW should be connected to inductor by wide and short trace. Keep sensitive components away from this trace.
- ▶ The R_T resistor, compensator and feedback components must be connected as close to the device as possible.

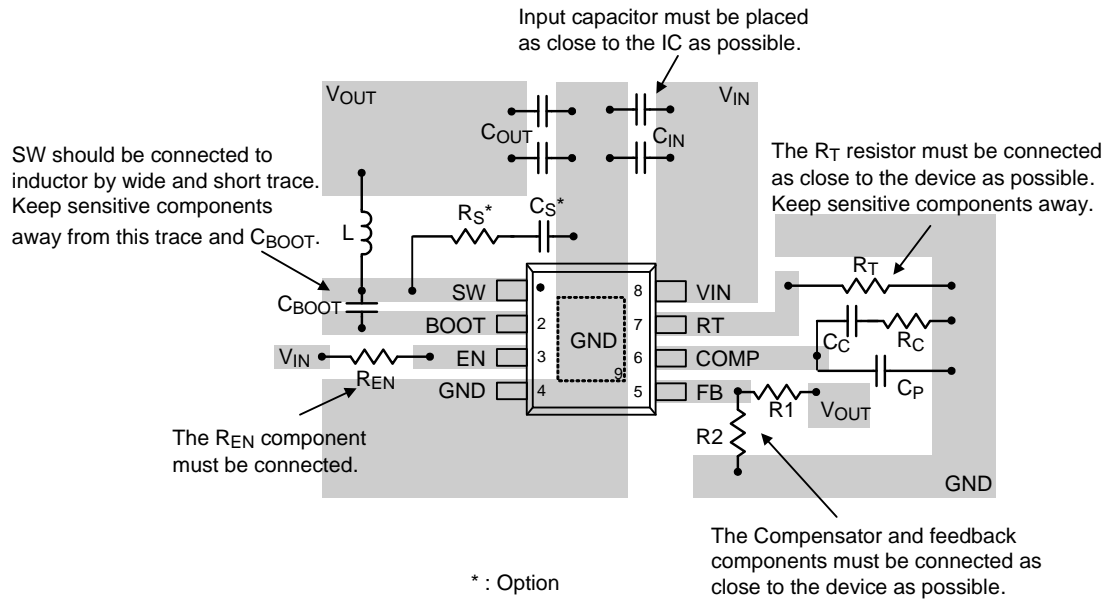
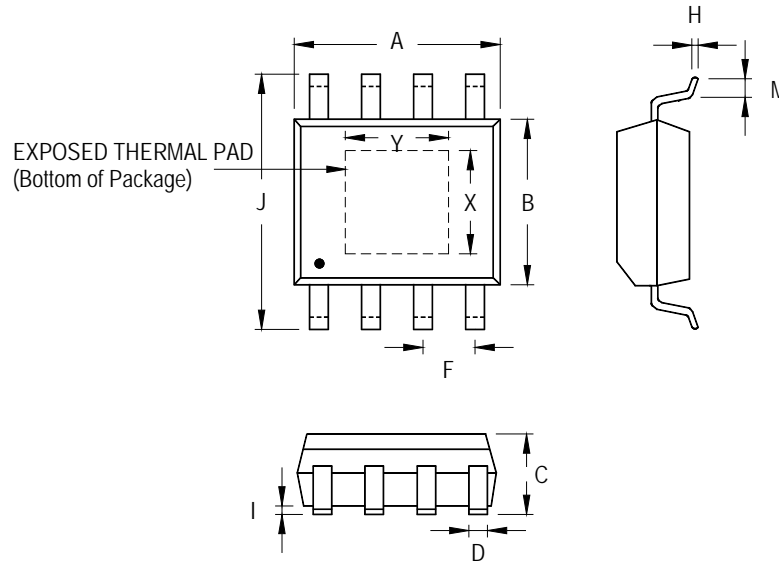


Figure 8. PCB Layout Guide

Table 3. Suggested Capacitors for CIN and COUT

Location	Component Supplier	Part No.	Capacitance (μF)	Case Size
CIN	MURATA	GRM32ER71H475K	4.7	1206
CIN	TAIYO YUDEN	UMK325BJ475MM-T	4.7	1206
CIN	MURATA	GRM31CR61E106K	10	1206
CIN	TDK	C3225X5R1E106K	10	1206
CIN	TAIYO YUDEN	TMK316BJ106ML	10	1206
COUT	MURATA	GRM31CR60J476M	47	1206
COUT	TDK	C3225X5R0J476M	47	1210
COUT	MURATA	GRM32ER71C226M	22	1210
COUT	TDK	C3225X5R1C22M	22	1210

Outline Dimension



Symbol	Dimensions In Millimeters		Dimensions In Inches		
	Min	Max	Min	Max	
A	4.801	5.004	0.189	0.197	
B	3.810	4.000	0.150	0.157	
C	1.346	1.753	0.053	0.069	
D	0.330	0.510	0.013	0.020	
F	1.194	1.346	0.047	0.053	
H	0.170	0.254	0.007	0.010	
I	0.000	0.152	0.000	0.006	
J	5.791	6.200	0.228	0.244	
M	0.406	1.270	0.016	0.050	
Option 1	X	2.000	2.300	0.079	0.091
	Y	2.000	2.300	0.079	0.091
Option 2	X	2.100	2.500	0.083	0.098
	Y	3.000	3.500	0.118	0.138

8-Lead SOP (Exposed Pad) Plastic Package

Richtek Technology Corporation

14F, No. 8, Tai Yuen 1st Street, Chupei City
 Hsinchu, Taiwan, R.O.C.
 Tel: (8863)5526789

Richtek products are sold by description only. Richtek reserves the right to change the circuitry and/or specifications without notice at any time. Customers should obtain the latest relevant information and data sheets before placing orders and should verify that such information is current and complete. Richtek cannot assume responsibility for use of any circuitry other than circuitry entirely embodied in a Richtek product. Information furnished by Richtek is believed to be accurate and reliable. However, no responsibility is assumed by Richtek or its subsidiaries for its use; nor for any infringements of patents or other rights of third parties which may result from its use. No license is granted by implication or otherwise under any patent or patent rights of Richtek or its subsidiaries.