

# 2A, 5.5V, Low I<sub>Q</sub> ACOT Synchronous Step-Down Converter

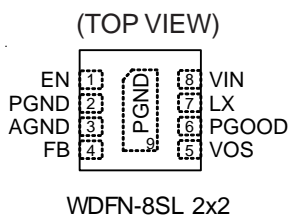
## General Description

The RT5795A is a full featured 5.5V, 2A, Advanced Constant-On-Time (ACOT) synchronous step-down converter with two integrated MOSFETs. The advanced COT operation allows transient responses to be optimized over a wide range of loads, and output capacitors to efficiently reduce external component count. The RT5795A provides up to 2.7MHz switching frequency to minimize the size of output inductor and capacitors. The RT5795A is available in the WDFN-8SL 2x2 package.

## Applications

- Mobile Phones and Handheld Devices
- STB, Cable Modem, and xDSL Platforms
- WLANASIC Power / Storage (SSD and HDD)
- General Purpose for POL LV Buck Converter

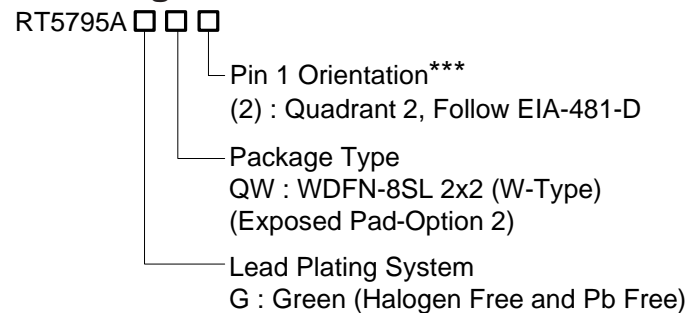
## Pin Configuration



## Features

- 2.5V to 5.5V Input Voltage Range
- Advanced COT Control loop design
- Fast Transient Response
- Internal 100mΩ and 80mΩ Synchronous Rectifier
- Highly Accurate V<sub>OUT</sub> Regulation Over Load/Line Range
- Robust Loop Stability with Low-ESR C<sub>OUT</sub>

## Ordering Information



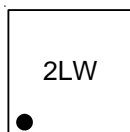
Note :

\*\*\*Empty means Pin1 orientation is Quadrant 1

Richtek products are :

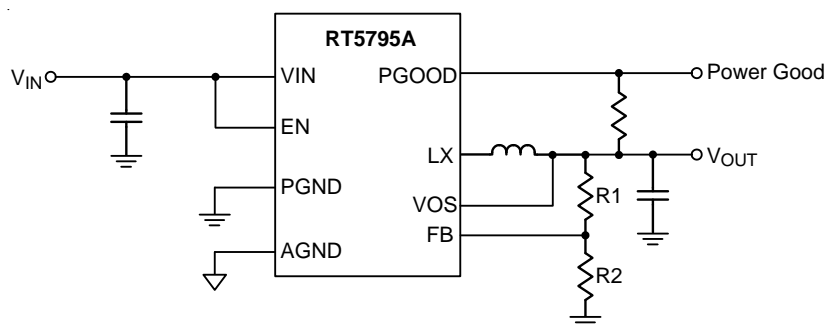
- ▶ RoHS compliant and compatible with the current requirements of IPC/JEDEC J-STD-020.
- ▶ Suitable for use in SnPb or Pb-free soldering processes.

## Marking Information



2L : Product Code  
W : Date Code

## Simplified Application Circuit





## Operation

The RT5795A is a low voltage synchronous step-down converter that can support input voltage ranging from 2.5V to 5.5V and the output current can be up to 2A. The RT5795A uses ACOT™ mode control. To achieve good stability with low-ESR ceramic capacitors, the ACOT uses a virtual inductor current ramp generated inside the IC. This internal ramp signal replaces the ESR ramp normally provided by the output capacitor's ESR. The ramp signal and other internal compensations are optimized for low-ESR ceramic output capacitors.

In steady-state operation, the feedback voltage, with the virtual inductor current ramp added, is compared to the reference voltage. When the combined signal is less than the reference, the on-time one-shot is triggered, as long as the minimum off-time one-shot is clear and the measured inductor current (through the synchronous rectifier) is below the current limit. The on-time one-shot turns on the high-side switch and the inductor current ramps up linearly. After the on-time, the high-side switch is turned off and the synchronous rectifier is turned on and the inductor current ramps down linearly. At the same time, the minimum off-time one-shot is triggered to prevent another immediate on-time during the noisy switching time and allow the feedback voltage and current sense signals to settle. The minimum off-time is kept short so that rapidly-repeated on-times can raise the inductor current quickly when needed.

### PWM Frequency and Adaptive On-Time Control

The on-time can be roughly estimated by the equation :

$$T_{ON} = \frac{V_{OUT}}{V_{IN}} \times \frac{1}{f_{OSC}} \text{ where } f_{OSC} \text{ is nominal } 2.7\text{MHz}$$

### Under-Voltage Protection (UVLO)

The UVLO continuously monitors the VCC voltage to make sure the device works properly. When the VCC is high enough to reach the UVLO high threshold voltage, the step-down converter softly starts or pre-bias to its regulated output voltage. When the VCC decreases to its low threshold voltage, the device shuts down.

### Power Good

When the output voltage is higher than PGOOD rising threshold, the PGOOD flag is high.

### Output Under-Voltage Protection (UVP)

When the output voltage is lower than 66% reference voltage after soft-start, the UVP is triggered.

### Over-Current Protection (OCP)

The RT5795A senses the current signal when the high-side and low-side MOSFET turns on. As a result, The OCP is a cycle-by-cycle current limit. If an over-current condition occurs, the converter turns off the next on pulse until inductor current drops below the OCP limit. If the OCP is continually activated and the load current is larger than the current provided by the converter, the output voltage drops. Also, when the output voltage triggers the UVP also, the current will drop to ZC and trigger the re-soft start sequence.

### Soft-Start

An internal current source charges an internal capacitor to build the soft-start ramp voltage. The typical soft-start time is 150µs.

### Over-Temperature Protection (OTP)

The RT5795A has an over-temperature protection. When the device triggers the OTP, the device shuts down until the temperature is back to normal.

## Absolute Maximum Ratings (Note 1)

- Supply Input Voltage,  $V_{IN}$  ----- -0.3V to 6V
- Switch Voltage,  $V_{LX}$  ----- -0.3V to 6V  
   < 50ns ----- -2.5V to 7V
- Other Pins ----- -0.3V to 6V
- Power Dissipation,  $P_D$  @  $T_A = 25^\circ\text{C}$   
   WDFN-8SL 2x2 ----- 1.538W
- Package Thermal Resistance (Note 2)  
   WDFN-8SL 2x2,  $\theta_{JA}$  -----  $65^\circ\text{C/W}$   
   WDFN-8SL 2x2,  $\theta_{JC}$  -----  $8^\circ\text{C/W}$
- Junction Temperature -----  $150^\circ\text{C}$
- Lead Temperature (Soldering, 10 sec.) -----  $260^\circ\text{C}$
- Storage Temperature Range -----  $-65^\circ\text{C}$  to  $150^\circ\text{C}$
- ESD Susceptibility (Note 3)  
   HBM (Human Body Model) ----- 2kV

## Recommended Operating Conditions (Note 4)

- Supply Input Voltage,  $V_{IN}$  ----- 2.5V to 5.5V
- Junction Temperature Range -----  $-40^\circ\text{C}$  to  $125^\circ\text{C}$
- Ambient Temperature Range -----  $-40^\circ\text{C}$  to  $85^\circ\text{C}$

## Electrical Characteristics

( $V_{IN} = 3.6\text{V}$ ,  $T_A = 25^\circ\text{C}$ , unless otherwise specified)

Parameter	Symbol	Test Conditions	Min	Typ	Max	Unit	
Under-Voltage Lockout Threshold	$V_{UVLO}$	$V_{CC}$ rising	2.28	2.35	2.48	V	
Under-Voltage Lockout Hysteresis	$V_{UVLOHY}$		--	400	--	mV	
Shutdown Supply Current	$I_{SHDN}$	$EN = 0\text{V}$	--	--	1	$\mu\text{A}$	
Quiescent Current	$I_Q$	Active, $V_{FB} = 0.5\text{V}$ , no switching	--	30	--	$\mu\text{A}$	
Voltage Reference	$V_{REF}$		0.441	0.45	0.459	V	
Current Limit	High-Side	$I_{LIM}$	Peak current	2.5	3.2	4	A
	Low-Side		Valley current	2	2.4	2.9	
Power Good Threshold	$V_{PGTH}$	$V_{OUT}$ falling referenced to $V_{OUT}$ nominal	-15	-10	-5	%	
Power Good Hysteresis	$V_{PGHY}$	Hysteresis referenced to $V_{OUT}$ nominal	--	5	--	%	
Power Good Leakage Current	$I_{PG}$	$V_{PG} = 5\text{V}$	--	0.01	0.1	$\mu\text{A}$	
Power Good Low Level Voltage	$V_{PGL}$	$I_{sink} = 500\mu\text{A}$	--	--	0.3	V	
Enable Rising Threshold	$V_{ENR}$	Rising	1	--	--	V	
Enable Falling Threshold	$V_{ENF}$	Falling	--	--	0.4	V	

Parameter		Symbol	Test Conditions	Min	Typ	Max	Unit
Switch On-Resistance	High-Side	R <sub>P</sub> -MOSFET		--	100	--	mΩ
	Low-Side	R <sub>N</sub> -MOSFET		--	80	--	
Thermal Shutdown Temperature				--	150	--	°C
Thermal Shutdown Hysteresis				--	20	--	°C
Switching Frequency		f <sub>osc</sub>		--	2.7	--	MHz
Output Discharge Resistor				--	1	--	kΩ

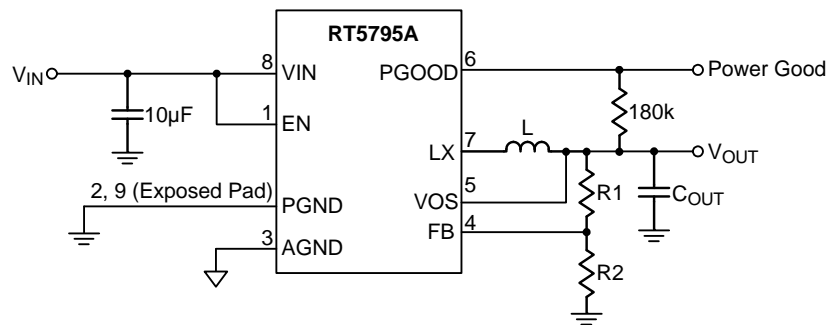
**Note 1.** Stresses beyond those listed under “Absolute Maximum Ratings” may cause permanent damage to the device. These are stress ratings only, and functional operation of the device at these or any other conditions beyond those indicated in the operational sections of the specifications is not implied. Exposure to absolute maximum rating conditions may affect device reliability.

**Note 2.**  $\theta_{JA}$  is measured at  $T_A = 25^\circ\text{C}$  on a high effective thermal conductivity four-layer test board per JEDEC 51-7.  $\theta_{JC}$  is measured at the exposed pad of the package. The copper area is  $70\text{mm}^2$  connected with IC exposed pad.

**Note 3.** Devices are ESD sensitive. Handling precaution is recommended.

**Note 4.** The device is not guaranteed to function outside its operating conditions.

## Typical Application Circuit

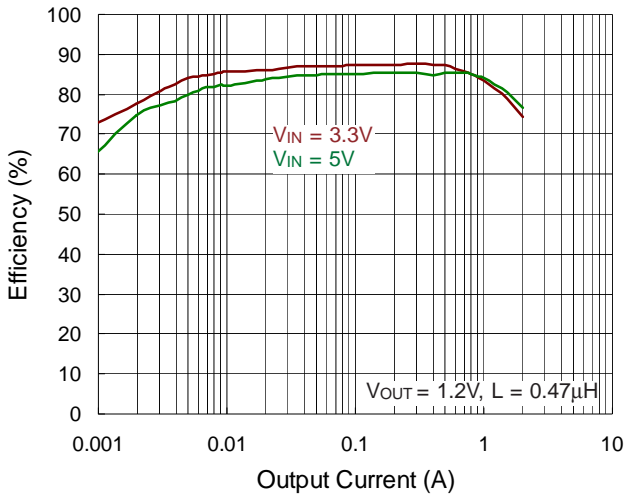


**Table 1. Suggested Component Values**

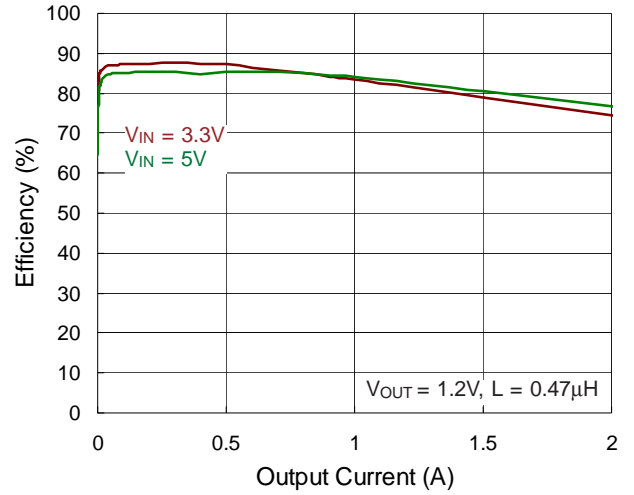
V <sub>OUT</sub> (V)	R <sub>1</sub> (kΩ)	R <sub>2</sub> (kΩ)	L (μH)	C <sub>OUT</sub> (μF)
1.2V	65.3	39.2	0.47	22
1.8V	117.6	39.2	1	22
2.5V	178.6	39.2	1	22
3.3V	248.3	39.2	1	22

**Typical Operating Characteristics**

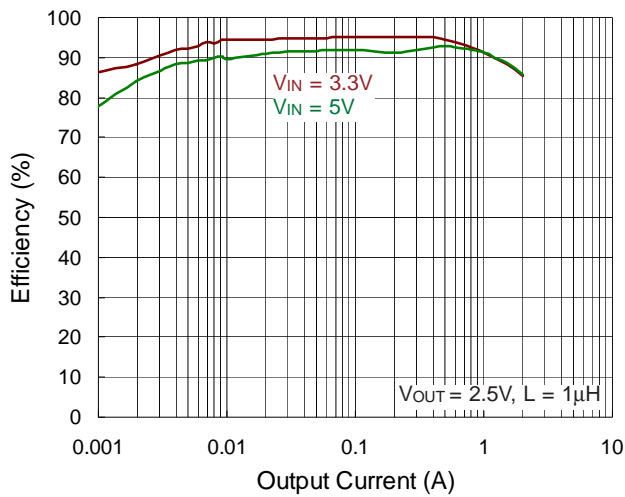
**Efficiency vs. Output Current**



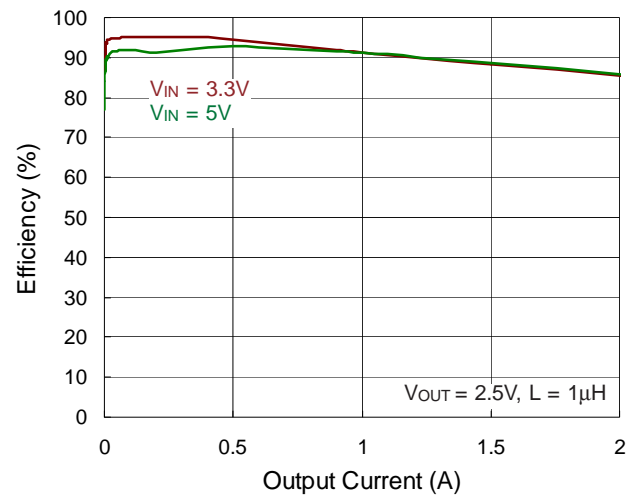
**Efficiency vs. Output Current**



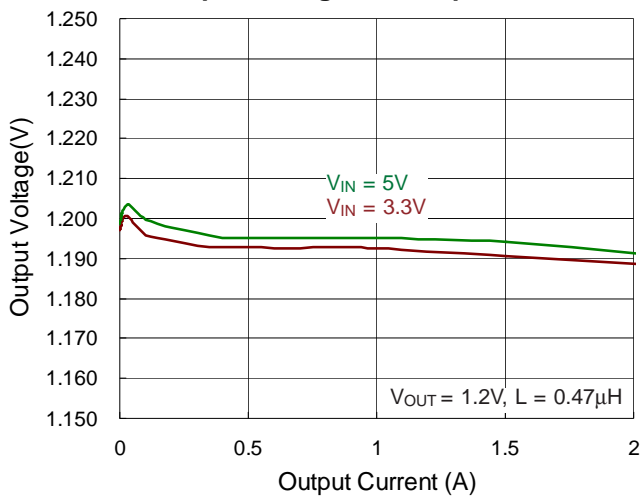
**Efficiency vs. Output Current**



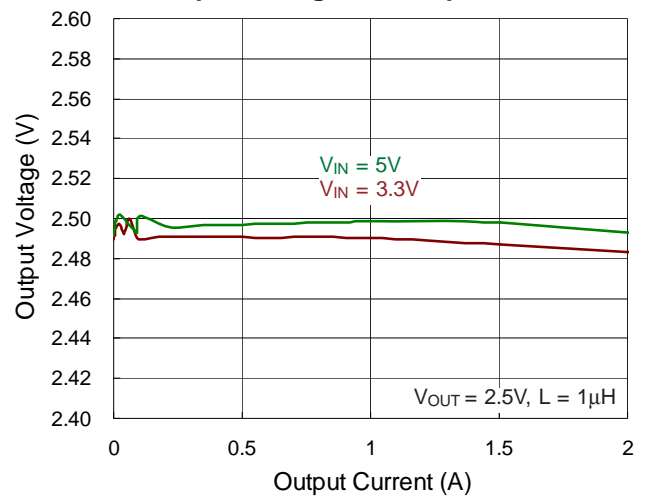
**Efficiency vs. Output Current**



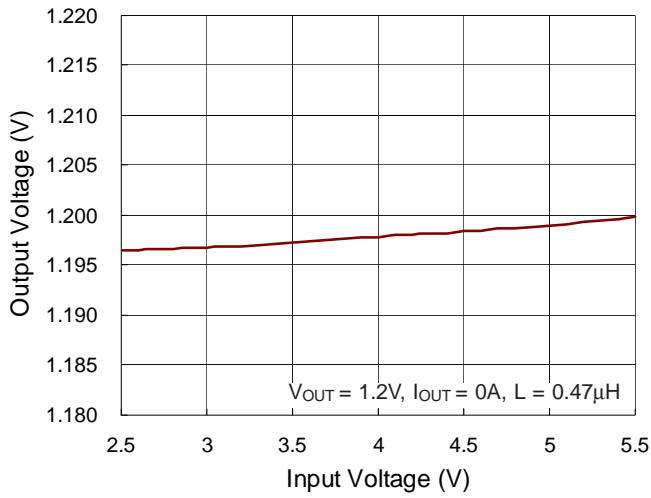
**Output Voltage vs. Output Current**



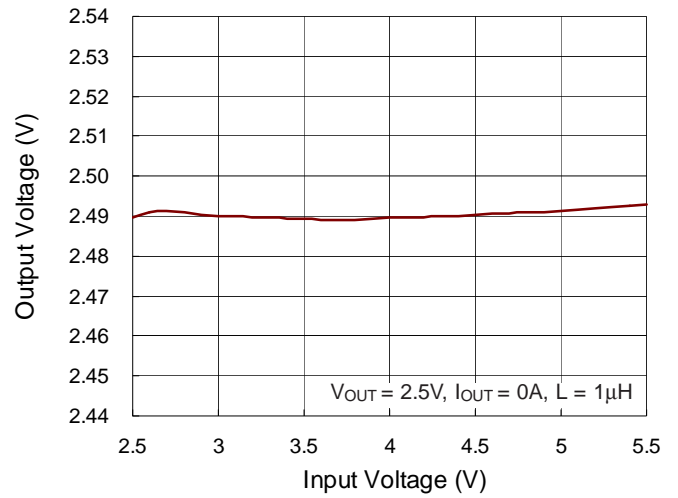
**Output Voltage vs. Output Current**



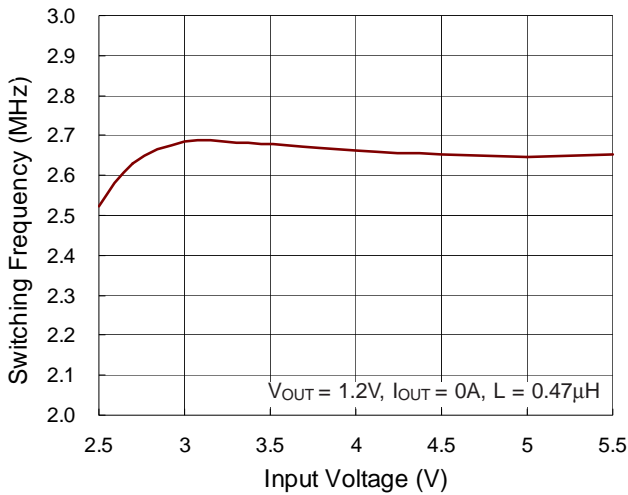
Output Voltage vs. Input Voltage



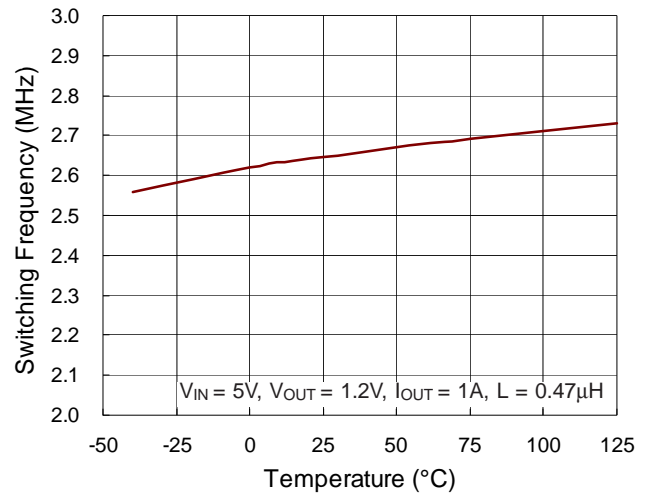
Output Voltage vs. Input Voltage



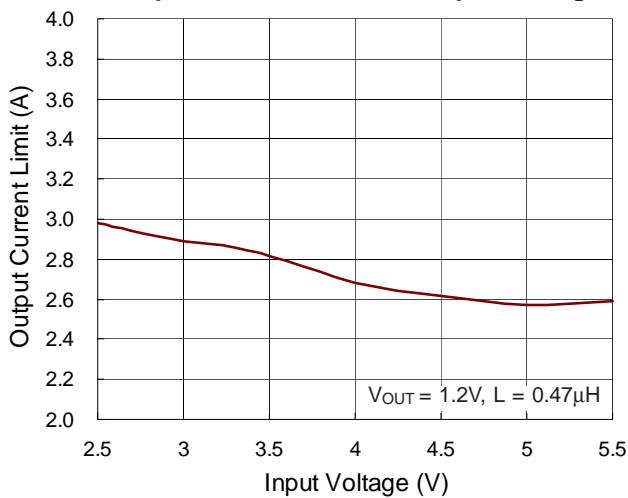
Switching Frequency vs. Input Voltage



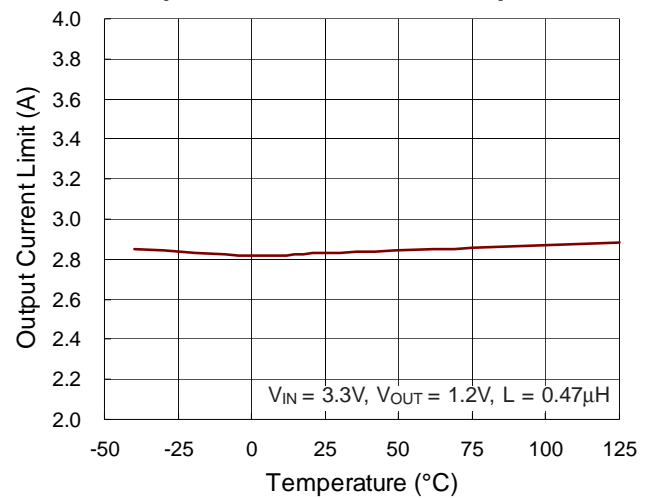
Switching Frequency vs. Temperature



Output Current Limit vs. Input Voltage

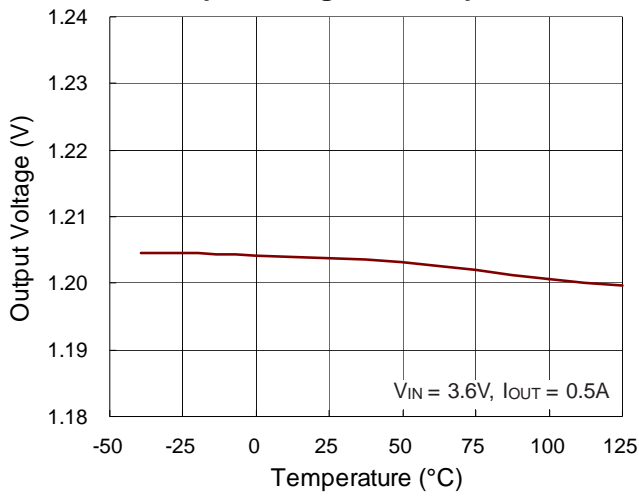


Output Current Limit vs. Temperature

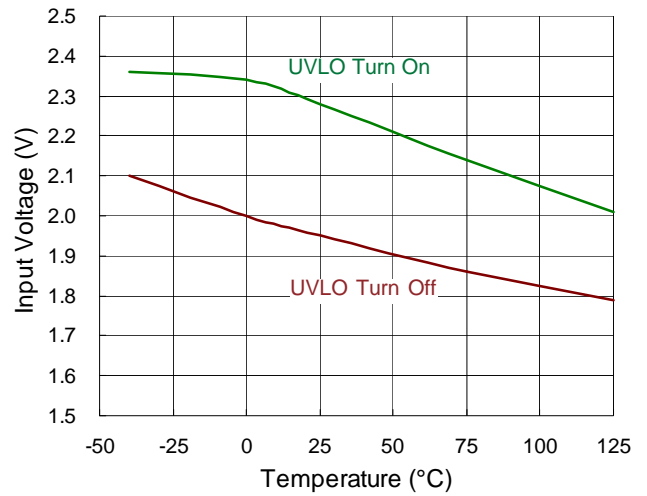




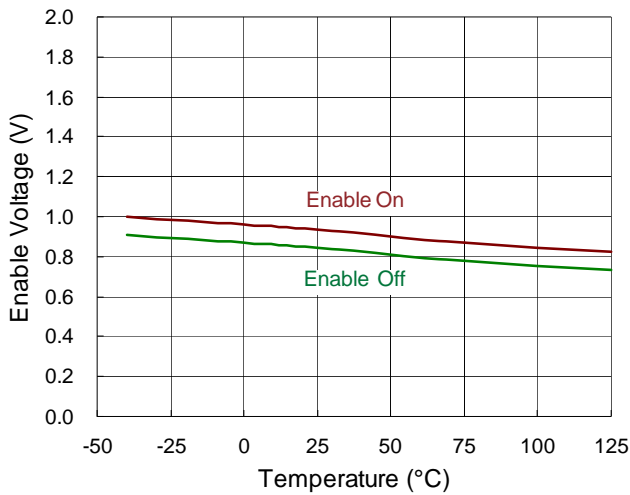
Output Voltage vs. Temperature



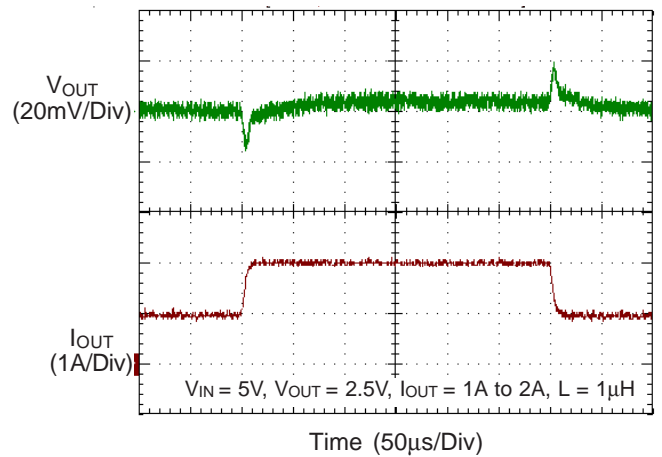
Input Voltage vs. Temperature



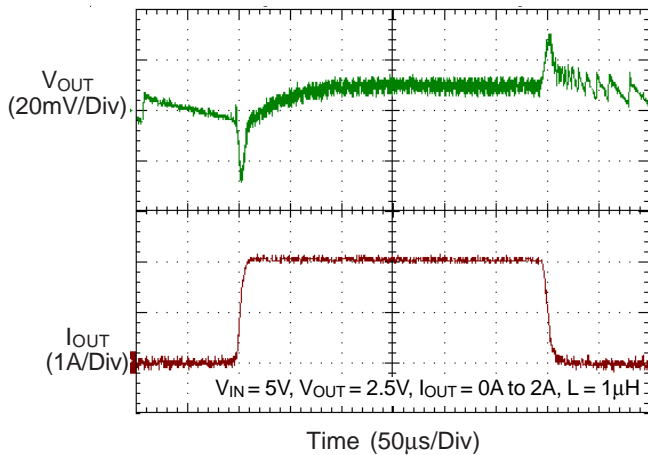
Enable Threshold vs. Temperature



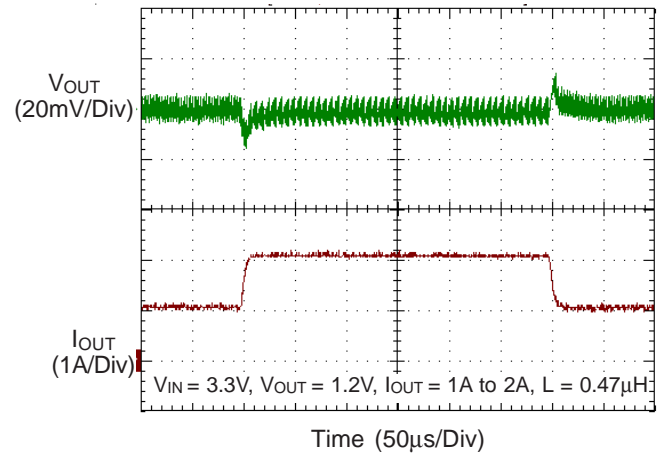
Load Transient Response



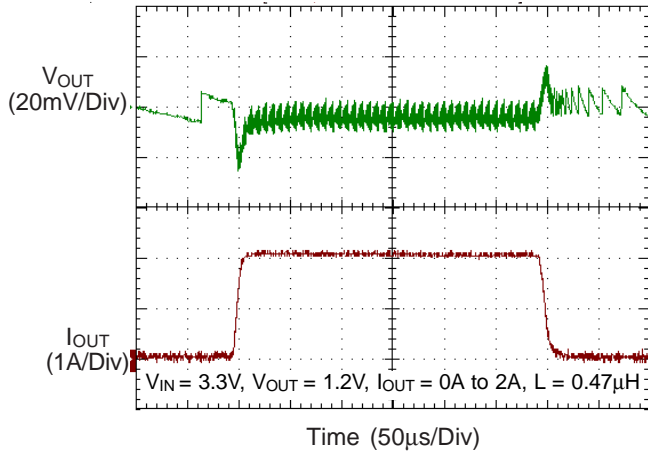
Load Transient Response



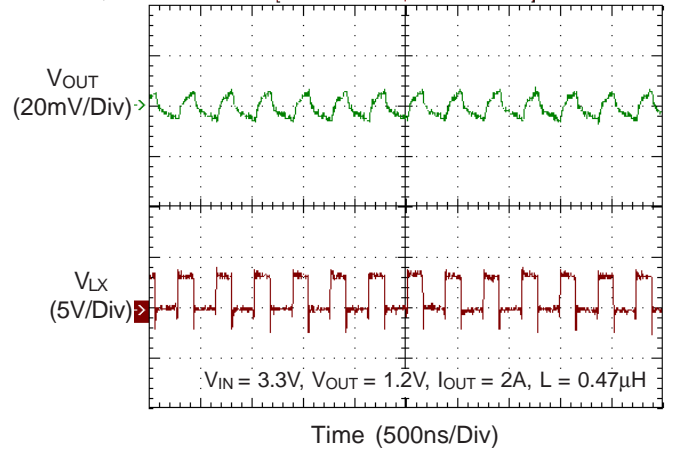
Load Transient Response



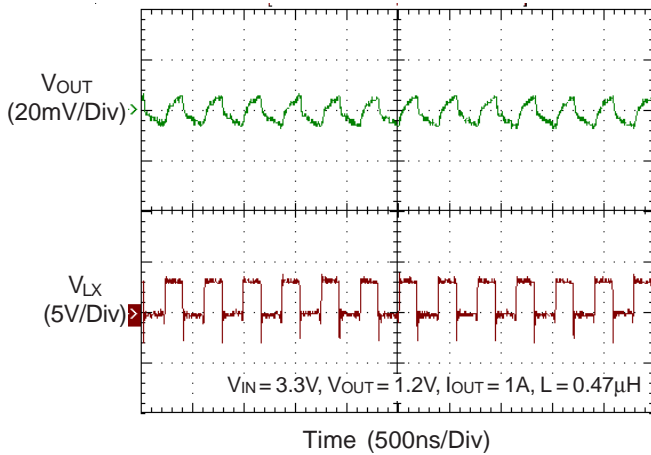
Load Transient Response



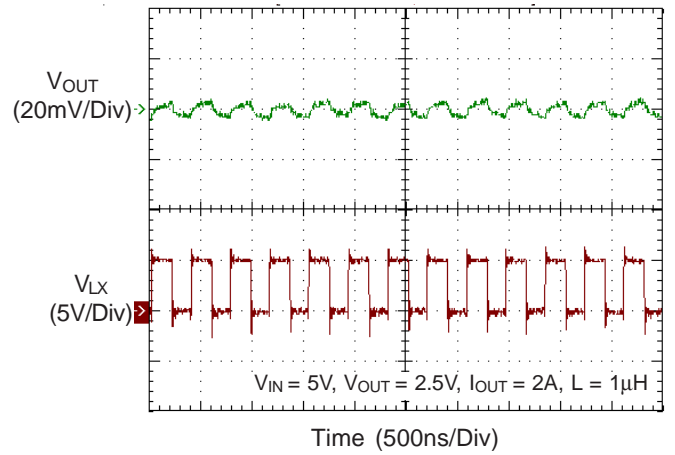
Voltage Ripple



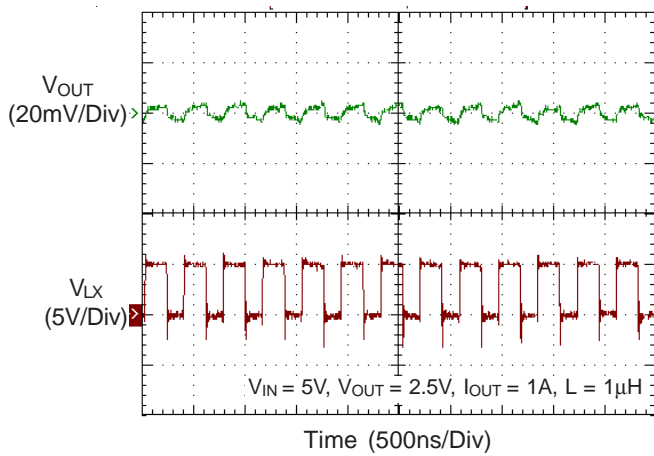
Voltage Ripple



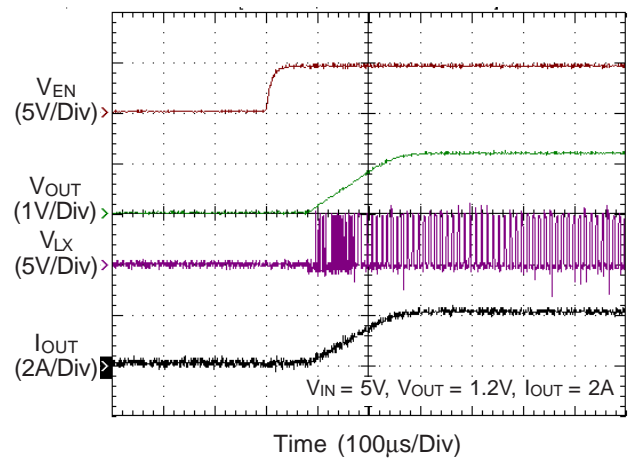
Voltage Ripple

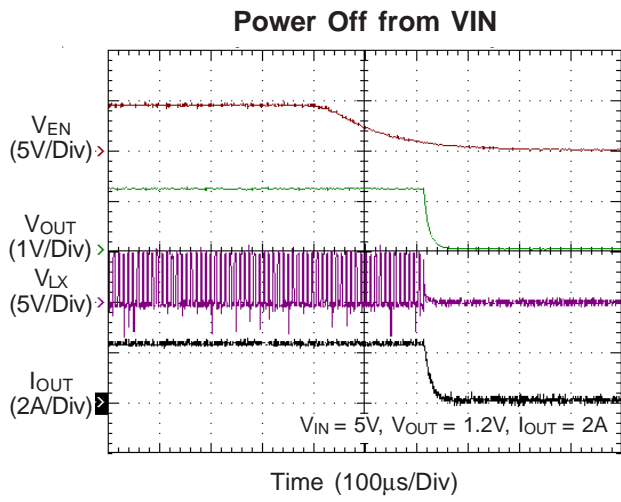


Voltage Ripple



Power On from VIN





## Application Information

The RT5795A is a single-phase step-down converter. Advance Constant-on-Time (ACOT) with fast transient response. An internal 0.45V reference allows the output voltage to be precisely regulated for low output voltage applications. A fixed switching frequency (2.7MHz) oscillator and internal compensation are integrated to minimize external component count. Protection features include over current protection, under voltage protection and over temperature protection.

### Output Voltage Setting

The output voltage is set by an external resistive divider according to the following equation :

$$V_{OUT} = V_{REF} \times \left(1 + \frac{R1}{R2}\right)$$

where VREF equals to 0.45V typical. The resistive divider allows the FB pin to sense a fraction of the output voltage as shown in Figure 1.

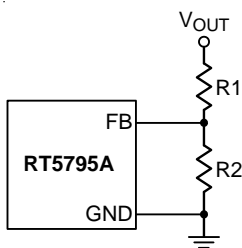


Figure 1. Setting the Output Voltage

### Low Supply Operation

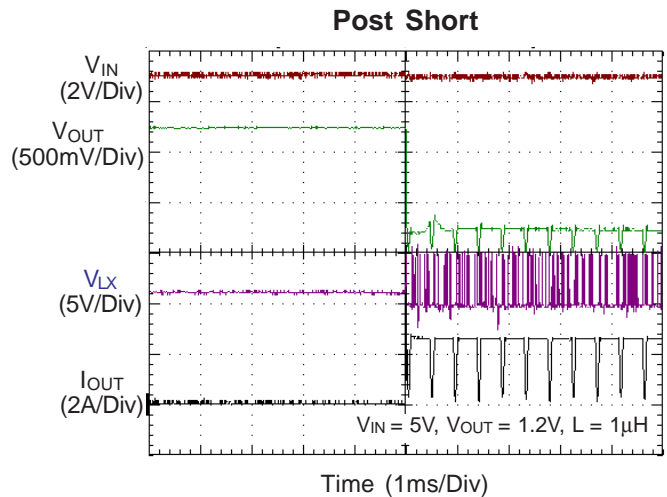
The RT5795A is designed to operate down to an input supply voltage of 2.5V. One important consideration at low input supply voltages is that the  $R_{DS(ON)}$  of the P-Channel and N-Channel power switches increases. The user should calculate the power dissipation when the RT5795A is used at 100% duty cycle with low input voltages to ensure that thermal limits are not exceeded.

### Under Voltage Protection (UVP)

#### Hiccup Mode

For the RT5795A, it provides Hiccup Mode Under Voltage Protection (UVP). When the output voltage is lower than 66% reference voltage after soft-start, the UVP is triggered. If the UVP condition remains for a period, the RT5795A

will retry automatically. When the UVP condition is removed, the converter will resume operation. The UVP is disabled during soft-start period.



### CIN and COUT Selection

The input capacitance,  $C_{IN}$ , is needed to filter the trapezoidal current at the source of the top MOSFET. To prevent large ripple voltage, a low ESR input capacitor sized for the maximum RMS current should be used. RMS current is given by :

$$I_{RMS} = I_{OUT(MAX)} \frac{V_{OUT}}{V_{IN}} \sqrt{\frac{V_{IN}}{V_{OUT}} - 1}$$

This formula has a maximum at  $V_{IN} = 2V_{OUT}$ , where  $I_{RMS} = I_{OUT} / 2$ . This simple worst case condition is commonly used for design because even significant deviations do not result in much difference. Choose a capacitor rated at a higher temperature than required.

Several capacitors may also be paralleled to meet size or height requirements in the design.

The selection of  $C_{OUT}$  is determined by the effective series resistance (ESR) that is required to minimize voltage ripple and load step transients, as well as the amount of bulk capacitance that is necessary to ensure that the control loop is stable. Loop stability can be checked by viewing the load transient response. The output ripple,  $\Delta V_{OUT}$ , is determined by :

$$\Delta V_{OUT} \leq \Delta I_L \left[ ESR + \frac{1}{8fC_{OUT}} \right]$$

The output ripple is highest at maximum input voltage since  $\Delta I_L$  increases with input voltage. Multiple capacitors placed in parallel may be needed to meet the ESR and RMS current handling requirements. Dry tantalum, special polymer, aluminum electrolytic and ceramic capacitors are all available in surface mount packages. Special polymer capacitors offer very low ESR, but have lower capacitance density than other types. Tantalum capacitors have the highest capacitance density, but it is important to only use types that have been surge tested for use in switching power supplies. Aluminum electrolytic capacitors have significantly higher ESR, but can be used in cost-sensitive applications provided that consideration is given to ripple current ratings and long term reliability. Ceramic capacitors have excellent low ESR characteristics, but can have a high voltage coefficient and audible piezoelectric effects. The high Q of ceramic capacitors with trace inductance can also lead to significant ringing.

**Using Ceramic Input and Output Capacitors**

Higher value, lower cost ceramic capacitors are now becoming available in smaller case sizes. Their high ripple current, high voltage rating and low ESR make them ideal for switching regulator applications. However, care must be taken when these capacitors are used at the input and output. When a ceramic capacitor is used at the input and the power is supplied by a wall adapter through long wires, a load step at the output can induce ringing at the input,  $V_{IN}$ . At best, this ringing can couple to the output and be mistaken as loop instability. At worst, a sudden inrush of current through the long wires can potentially cause a voltage spike at  $V_{IN}$  large enough to damage the part.

**Table 2. Capacitors for  $C_{IN}$  and  $C_{OUT}$**

Component Supplier	Part No.	Capacitance ( $\mu F$ )	Case Size
MuRata	GRM31CR71A106KA01	10 $\mu F$	1206
MuRata	GRM31CR71A226KA01	22 $\mu F$	1206

**Thermal Considerations**

For continuous operation, do not exceed absolute maximum junction temperature. The maximum power dissipation depends on the thermal resistance of the IC package, PCB layout, rate of surrounding airflow, and difference between junction and ambient temperature. The maximum power dissipation can be calculated by the following formula :

$$P_{D(MAX)} = (T_{J(MAX)} - T_A) / \theta_{JA}$$

where  $T_{J(MAX)}$  is the maximum junction temperature,  $T_A$  is the ambient temperature, and  $\theta_{JA}$  is the junction to ambient thermal resistance.

For recommended operating condition specifications, the maximum junction temperature is 125°C. The junction to ambient thermal resistance,  $\theta_{JA}$ , is layout dependent. The junction to ambient thermal resistance,  $\theta_{JA}$ , is layout dependent. For WDFN-8SL 2x2 packages, the thermal resistance,  $\theta_{JA}$ , is 65°C/W on a standard JEDEC 51-7 four-layer thermal test board. The maximum power dissipation at  $T_A = 25^\circ C$  can be calculated by the following formula :

$$P_{D(MAX)} = (125^\circ C - 25^\circ C) / (65^\circ C/W) = 1.538W \text{ for WDFN-8SL 2x2 package}$$

The maximum power dissipation depends on the operating ambient temperature for fixed  $T_{J(MAX)}$  and thermal resistance,  $\theta_{JA}$ . The derating curve in Figure 2 allows the designer to see the effect of rising ambient temperature on the maximum power dissipation.

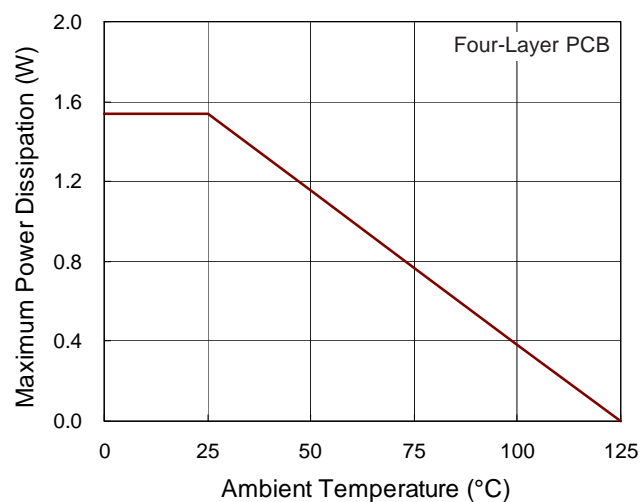


Figure 2. Derating Curve of Maximum Power Dissipation

## Layout Considerations

Follow the PCB layout guidelines for optimal performance of the RT5795A.

- ▶ Connect the terminal of the input capacitor(s),  $C_{IN}$ , as close as possible to the  $V_{IN}$  pin. This capacitor provides the AC current into the internal power MOSFETs.
- ▶ LX node experiences high frequency voltage swing and should be kept within a small area. Keep all sensitive small-signal nodes away from the LX node to prevent stray capacitive noise pick up.

- ▶ Flood all unused areas on all layers with copper. Flooding with copper will reduce the temperature rise of power components. Connect the copper areas to any DC net ( $V_{IN}$ ,  $V_{OUT}$ , GND, or any other DC rail in the system).
- ▶ Connect the FB pin directly to the feedback resistors. The resistive voltage divider must be connected between  $V_{OUT}$  and GND.

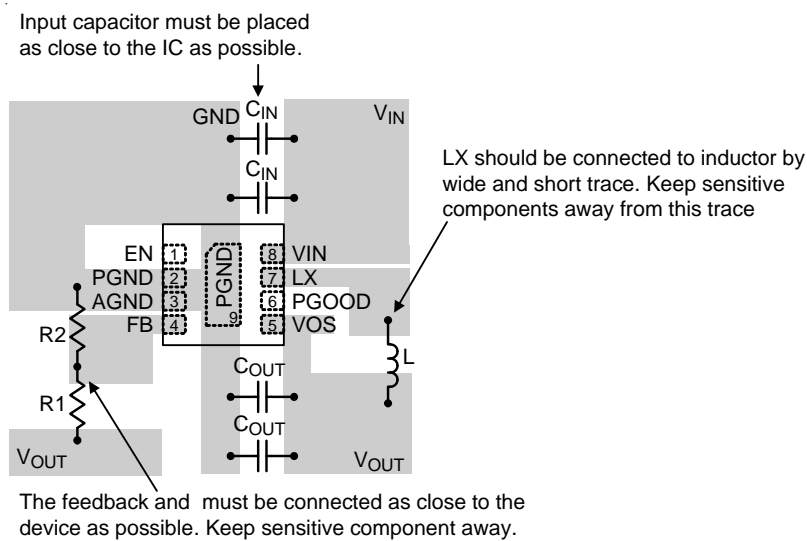
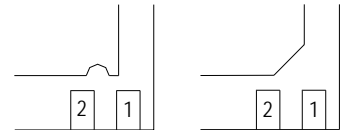
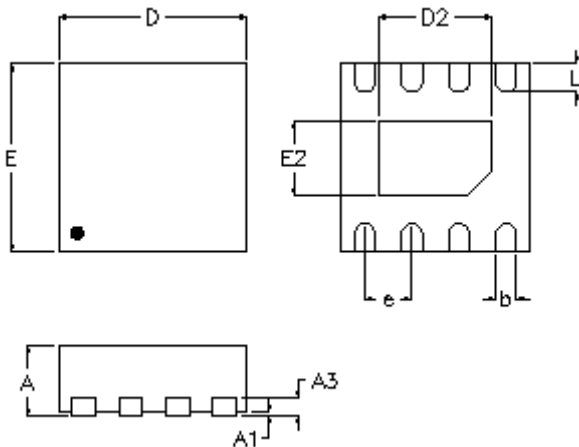


Figure 3. PCB Layout Guide

**Outline Dimension**



**DETAILA**

Pin #1 ID and Tie Bar Mark Options

Note : The configuration of the Pin #1 identifier is optional, but must be located within the zone indicated.

Symbol	Dimensions In Millimeters		Dimensions In Inches		
	Min.	Max.	Min.	Max.	
A	0.700	0.800	0.028	0.031	
A1	0.000	0.050	0.000	0.002	
A3	0.175	0.250	0.007	0.010	
b	0.200	0.300	0.008	0.012	
D	1.900	2.100	0.075	0.083	
D2	Option1	1.150	1.250	0.045	0.049
	Option2	1.550	1.650	0.061	0.065
E	1.900	2.100	0.075	0.083	
E2	Option1	0.750	0.850	0.030	0.033
	Option2	0.850	0.950	0.033	0.037
e	0.500		0.020		
L	0.250	0.350	0.010	0.014	

**W-Type 8SL DFN 2x2 Package**

**Richtek Technology Corporation**

14F, No. 8, Tai Yuen 1<sup>st</sup> Street, Chupei City  
 Hsinchu, Taiwan, R.O.C.  
 Tel: (8863)5526789

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